

be permitted for round or octagonal structural systems.

TY

K_d , shall be determined from the wind loads calculated in accordance with Chapter 31 shall of the wind speeds conforming 6.5.3 and of Section 31.4.3.

dered, the upwind exposure roughness that is determined vegetation, and constructed

ctors. For each selected wind ds are to be determined, the ructure shall be determined nding 45° on either side of exposure in these two sectors ith Sections 26.7.2 and 26.7.3, h would result in the highest resent the winds from that

egories. A ground surface : shall be determined for a ined in Section 26.7.3, from ving text, for the purpose of defined in Section 26.7.3. und suburban areas, wooded s, closely spaced obstructions dwellings or larger. rrain with scattered obstruc- ss than 30 ft (9.1 m). This / and grasslands. obstructed areas and water ooth mud flats, salt flats, and

categories, the category resulting in the largest wind forces shall be used.

EXCEPTION: An intermediate exposure between the preceding categories is permitted in a transition zone, provided that it is determined by a rational analysis method defined in the recognized literature.

26.7.4 Exposure Requirements.

26.7.4.1 Directional Procedure (Chapter 27). For each wind direction considered, wind loads for the design of the MWFRS of enclosed and partially enclosed buildings using the Directional Procedure of Chapter 27 shall be based on the exposures as defined in Section 26.7.3. Wind loads for the design of open buildings with monoslope, pitched, or troughed free roofs shall be based on the exposures, as defined in Section 26.7.3, resulting in the highest wind loads for any wind direction at the site.

26.7.4.2 Envelope Procedure (Chapter 28). Wind loads for the design of the MWFRS for all low-rise buildings designed using the Envelope Procedure of Chapter 28 shall be based on the exposure category resulting in the highest wind loads for any wind direction at the site.

26.7.4.3 Directional Procedure for Building Appurtenances and Other Structures (Chapter 29). Wind loads for the design of building appurtenances (such as rooftop structures and equipment) and other structures (such as solid freestanding walls and freestanding signs, chimneys, tanks, open signs, single-plane open frames, and trussed towers) as specified in Chapter 29 shall be based on the appropriate exposure for each wind direction considered.

26.7.4.4 Components and Cladding (Chapter 30). Design wind pressures for C&C shall be based on the exposure category resulting in the highest wind loads for any wind direction at the site.

26.8 TOPOGRAPHIC EFFECTS

26.8.1 Wind Speed-Up over Hills, Ridges, and Escarpments. Wind speed-up effects at isolated hills, ridges, and escarpments constituting abrupt changes in the general topography, located in any exposure category, shall be included in the determination of the wind loads when site

conditions and locations of buildings and other structures meet all of the following conditions:

1. The hill, ridge, or escarpment is isolated and unobstructed upwind by other similar topographic features of comparable height for 100 times the height of the topographic feature ($100H$) or 2 mi (3.22 km), whichever is less. This distance shall be measured horizontally from the point at which the height H of the hill, ridge, or escarpment is determined.
2. The hill, ridge, or escarpment protrudes above the height of upwind terrain features within a 2-mi (3.22-km) radius in any quadrant by a factor of 2 or more.
3. The building or other structure is located as shown in Fig. 26.8-1 in the upper one-half of a hill or ridge or near the crest of an escarpment.
4. $H/L_h \geq 0.2$.
5. H is greater than or equal to 15 ft (4.5 m) for Exposure C and D and 60 ft (18 m) for Exposure B.

26.8.2 Topographic Factor. The wind speed-up effect shall be included in the calculation of design wind loads by using the factor K_{zt} :

$$K_{zt} = (1 + K_1 K_2 K_3)^2 \quad (26.8-1)$$

where K_1 , K_2 , and K_3 are given in Fig. 26.8-1.

If site conditions and locations of buildings and other structures do not meet all the conditions specified in Section 26.8.1, then $K_{zt} = 1.0$.

26.9 GROUND ELEVATION FACTOR

The ground elevation factor to adjust for air density, K_e , shall be determined in accordance with Table 26.9-1. It is permitted to take $K_e = 1$ for all elevations.

26.10 VELOCITY PRESSURE

26.10.1 Velocity Pressure Exposure Coefficient. Based on the exposure category determined in Section 26.7.3, a velocity pressure exposure coefficient, K_z or K_h , as applicable, shall be determined from Table 26.10-1. For a site located in a transition zone between exposure categories that is near to a change in ground surface roughness, intermediate values of K_z or K_h ,

Table 26.9-1 Ground Elevation Factor, K_e

Ground Elevation above Sea Level		Ground Elevation Factor K_e
ft	m	
<0	<0	See note 2
0	0	1.00
1,000	305	0.96
2,000	610	0.93
3,000	914	0.90
4,000	1,219	0.86
5,000	1,524	0.83
6,000	1,829	0.80
>6,000	>1,829	See note 2

Notes

1. The conservative approximation $K_e = 1.00$ is permitted in all cases.
2. The factor K_e shall be determined from the above table using interpolation or from the following formula for all elevations:
 $K_e = e^{-0.0000362z_g}$ (z_g = ground elevation above sea level in ft)
 $K_e = e^{-0.000119z_g}$ (z_g = ground elevation above sea level in m).
3. K_e is permitted to be taken as 1.00 in all cases.

Table 26.10-1 Velocity Pressure Exposure Coefficients, K_h and K_z

Height above Ground Level, z		Exposure		
ft	m	B	C	D
0-15	0-4.6	0.57 (0.70) ^a	0.85	1.03
20	6.1	0.62 (0.70) ^a	0.90	1.08
25	7.6	0.66 (0.70) ^a	0.94	1.12
30	9.1	0.70	0.98	1.16
40	12.2	0.76	1.04	1.22
50	15.2	0.81	1.09	1.27
60	18.0	0.85	1.13	1.31
70	21.3	0.89	1.17	1.34
80	24.4	0.93	1.21	1.38
90	27.4	0.96	1.24	1.40
100	30.5	0.99	1.26	1.43
120	36.6	1.04	1.31	1.48
140	42.7	1.09	1.36	1.52
160	48.8	1.13	1.39	1.55
180	54.9	1.17	1.43	1.58
200	61.0	1.20	1.46	1.61
250	76.2	1.28	1.53	1.68
300	91.4	1.35	1.59	1.73
350	106.7	1.41	1.64	1.78
400	121.9	1.47	1.69	1.82
450	137.2	1.52	1.73	1.86
500	152.4	1.56	1.77	1.89

^aUse 0.70 in Chapter 28, Exposure B, when $z < 30$ ft (9.1 m).

Notes

1. The velocity pressure exposure coefficient K_z may be determined from the following formula:
For 15 ft (4.6 m) $\leq z \leq z_g$ $K_z = 2.01(z/z_g)^{2/\alpha}$
For $z < 15$ ft (4.6 m) $K_z = 2.01(15/z_g)^{2/\alpha}$
2. α and z_g are tabulated in Table 26.11-1.
3. Linear interpolation for intermediate values of height z is acceptable.
4. Exposure categories are defined in Section 26.7.

between those shown in Table 26.10-1 are permitted provided that they are determined by a rational analysis method defined in the recognized literature.

26.10.2 Velocity Pressure. Velocity pressure, q_z , evaluated at height z above ground shall be calculated by the following equation:

$$q_z = 0.00256 K_z K_{zt} K_d K_e V^2 \quad (\text{lb/ft}^2); \quad V \text{ in mi/h} \quad (26.10-1)$$

$$q_z = 0.613 K_z K_{zt} K_d K_e V^2 \quad (\text{N/m}^2); \quad V \text{ in m/s} \quad (26.10-1a)$$

where

- K_z = velocity pressure exposure coefficient, see Section 26.10.1.
- K_{zt} = topographic factor, see Section 26.8.2.
- K_d = wind directionality factor, see Section 26.6.
- K_e = ground elevation factor, see Section 26.9.
- V = basic wind speed, see Section 26.5.
- q_z = velocity pressure at height z .

The velocity pressure at mean roof height is computed as $q_h = q_z$ evaluated from Eq. (26.10-1) using K_z at mean roof height h .

The basic wind speed, V , used in determination of design wind loads on rooftop structures, rooftop equipment, and other